

1.1nV/ $\sqrt{\text{Hz}}$ Noise, Low Power, Precision Operational Amplifier in Small DFN-8 Package

FEATURES

- **LOW VOLTAGE NOISE:** 1.1nV/ $\sqrt{\text{Hz}}$ at 1kHz
- **INPUT VOLTAGE NOISE:** 80nV_{PP} (0.1Hz to 10Hz)
- **THD+N:** -136dB (G = 1, f = 1kHz)
- **OFFSET VOLTAGE:** 125 μV (max)
- **OFFSET VOLTAGE DRIFT:** 0.35 $\mu\text{V}/^\circ\text{C}$ (typ)
- **LOW SUPPLY CURRENT:** 3.6mA/Ch (typ)
- **UNITY GAIN STABLE**
- **GAIN BANDWIDTH PRODUCT:** 80MHz (G = 100)
45MHz (G = 1)
- **SLEW RATE:** 27V/ μs
- **16-BIT SETTling:** 700ns
- **WIDE SUPPLY RANGE:** $\pm 2.25\text{V}$ to $\pm 18\text{V}$, +4.5V to +36V
- **RAIL-TO-RAIL OUTPUT**
- **OUTPUT CURRENT:** 30mA
- **DFN-8 (3 \times 3mm), MSOP-8, AND SO-8**

APPLICATIONS

- PLL LOOP FILTER
- LOW-NOISE, LOW-POWER SIGNAL PROCESSING
- 16-BIT ADC DRIVERS
- DAC OUTPUT AMPLIFIER
- ACTIVE FILTERS
- LOW-NOISE INSTRUMENTATION AMPS
- ULTRASOUND AMPLIFIERS
- PROFESSIONAL AUDIO PREAMPLIFIERS
- LOW-NOISE FREQUENCY SYNTHESIZERS
- INFRARED DETECTOR AMPLIFIERS
- HYDROPHONE AMPLIFIERS
- GEOPHONE AMPLIFIERS
- MEDICAL

DESCRIPTION

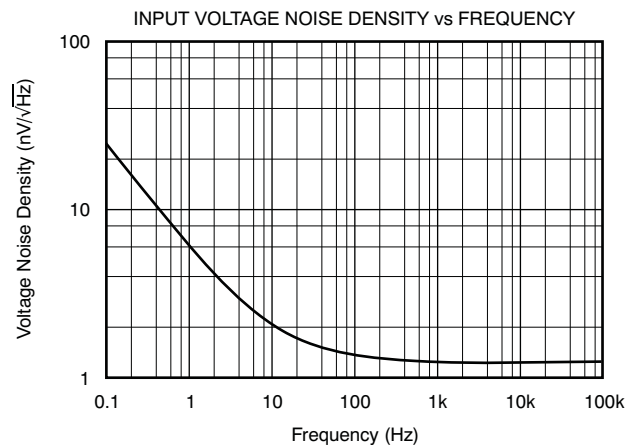
The OPA211 series of precision operational amplifiers achieves very low 1.1nV/ $\sqrt{\text{Hz}}$ noise density with a supply current of only 3.6mA. This series also offers rail-to-rail output swing, which maximizes dynamic range.

The extremely low voltage and low current noise, high speed, and wide output swing of the OPA211 series make these devices an excellent choice as a loop filter amplifier in PLL applications.

In precision data acquisition applications, the OPA211 series of op amps provides 700ns settling time to 16-bit accuracy throughout 10V output swings. This ac performance, combined with only 125 μV of offset and 0.35 $\mu\text{V}/^\circ\text{C}$ of drift over temperature, makes the OPA211 ideal for driving high-precision 16-bit analog-to-digital converters (ADCs) or buffering the output of high-resolution digital-to-analog converters (DACs).

The OPA211 series is specified over a wide dual-power supply range of $\pm 2.25\text{V}$ to $\pm 18\text{V}$, or single-supply operation from +4.5V to +36V.

The OPA211 is available in the small DFN-8 (3 \times 3mm), MSOP-8, and SO-8 packages. A dual version, the OPA2211, is available in the DFN-8 (3 \times 3mm) or an SO-8 PowerPAD™ package. This series of op amps is specified from $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$.



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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

ABSOLUTE MAXIMUM RATINGS⁽¹⁾

Over operating free-air temperature range (unless otherwise noted).

		VALUE	UNIT
Supply Voltage	$V_S = (V+) - (V-)$	40	V
Input Voltage		$(V-) - 0.5$ to $(V+) + 0.5$	V
Input Current (Any pin except power-supply pins)		± 10	mA
Output Short-Circuit ⁽²⁾		Continuous	
Operating Temperature	(T_A)	-55 to +150	°C
Storage Temperature	(T_A)	-65 to +150	°C
Junction Temperature	(T_J)	200	°C
ESD Ratings	Human Body Model (HBM)	3000	V
	Charged Device Model (CDM)	1000	V

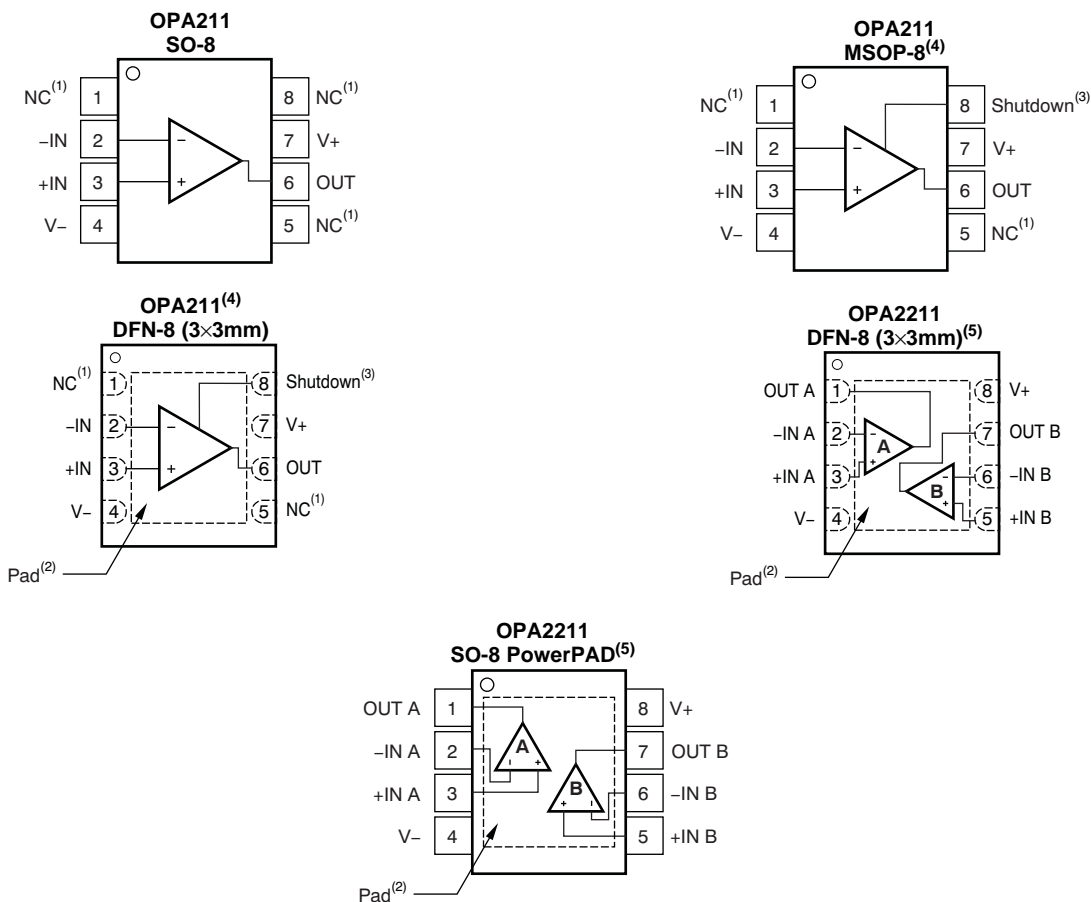
- (1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not supported.
- (2) Short-circuit to $V_S/2$ (ground in symmetrical dual supply setups), one amplifier per package.

PACKAGE/ORDERING INFORMATION⁽¹⁾

PRODUCT	PACKAGE-LEAD	SINGLE	SHUTDOWN	DUAL	PACKAGE DESIGNATOR	PACKAGE MARKING
Standard Grade						
OPA211AI	DFN-8 (3×3mm) ⁽²⁾	✓	✓		DRG	OB DQ
	MSOP-8 ⁽²⁾	✓	✓		DGK	OBCQ
OPA211AI	SO-8	✓			D	A TI OPA 211
OPA2211AI	DFN-8 (3×3mm) ⁽³⁾			✓	DRG	OBHQ
	SO-8 PowerPAD ⁽³⁾			✓	DDA	A TI OPA 2211
High Grade⁽³⁾						
OPA211I	DFN-8 (3×3mm)	✓	✓		DRG	OB D Q
	MSOP-8	✓	✓		DGK	OBCQ
	SO-8	✓			D	TI OPA 211
OPA2211I	DFN-8 (3×3mm)			✓	DRG	OBHQ
	SO-8 PowerPAD			✓	DDA	TI OPA 2211

- (1) For the most current package and ordering information see the Package Option Addendum at the end of this document, or see the TI web site at www.ti.com.
- (2) Available Q2, 2008.
- (3) Available Q3, 2008.

PIN CONFIGURATIONS



- (1) NC denotes no internal connection. Pin can be left floating or connected to any voltage between (V-) and (V+).
- (2) Exposed thermal die pad on underside; connect thermal die pad to V-.
- (3) Shutdown function:
 - Device enabled: $(V-) \leq V_{SHUTDOWN} \leq (V+) - 3V$
 - Device disabled: $V_{SHUTDOWN} \geq (V+) - 0.35V$
- (4) Available Q2, 2008.
- (5) Available Q3, 2008.

ELECTRICAL CHARACTERISTICS: $V_S = \pm 2.25V$ to $\pm 18V$

BOLDFACE limits apply over the specified temperature range, $T_A = -40^\circ C$ to $+125^\circ C$.

At $T_A = +25^\circ C$ and $R_L = 10k\Omega$, unless otherwise noted.

PARAMETER	CONDITIONS	Standard Grade OPA211A, OPA2211A			UNIT
		MIN	TYP	MAX	
OFFSET VOLTAGE					
Input Offset Voltage	V_{OS} $V_S = \pm 15V$		± 30	± 125	μV
Drift vs Power Supply Over Temperature	dV_{OS}/dT PSRR $V_S = \pm 2.25V$ to $\pm 18V$		0.35 0.1	1 3	$\mu V/^\circ C$ $\mu V/V$ $\mu V/V$
INPUT BIAS CURRENT					
Input Bias Current Over Temperature	I_B $V_{CM} = 0V$		± 60	± 175 ± 200	nA nA
Offset Current Over Temperature	I_{OS} $V_{CM} = 0V$		± 25	± 100 ± 150	nA nA
NOISE					
Input Voltage Noise	e_n $f = 0.1Hz$ to $10Hz$		80		nV _{PP}
Input Voltage Noise Density	$f = 10Hz$ $f = 100Hz$ $f = 1kHz$		2 1.4 1.1		nV/ \sqrt{Hz} nV/ \sqrt{Hz} nV/ \sqrt{Hz}
Input Current Noise Density	i_n $f = 10Hz$ $f = 1kHz$		3.2 1.7		pA/ \sqrt{Hz} pA/ \sqrt{Hz}
INPUT VOLTAGE RANGE					
Common-Mode Voltage Range	V_{CM} $V_S \geq \pm 5V$ $V_S < \pm 5V$	$(V-) + 1.8$ $(V-) + 2$		$(V+) - 1.4$ $(V+) - 1.4$	V V
Common-Mode Rejection Ratio	CMRR $V_S \geq \pm 5V, (V-) + 2V \leq V_{CM} \leq (V+) - 2V$ $V_S < \pm 5V, (V-) + 2V \leq V_{CM} \leq (V+) - 2V$	114 110	120 120		dB dB
INPUT IMPEDANCE					
Differential			20k 8		Ω pF
Common-Mode			10 ⁹ 2		Ω pF
OPEN-LOOP GAIN					
Open-Loop Voltage Gain	A_{OL} $(V-) + 0.2V \leq V_O \leq (V+) - 0.2V,$ $R_L = 10k\Omega$	114	130		dB
	A_{OL} $(V-) + 0.6V \leq V_O \leq (V+) - 0.6V,$ $R_L = 600\Omega$	110	114		dB
Over Temperature	A_{OL} $(V-) + 0.6V \leq V_O \leq (V+) - 0.6V,$ $I_O \leq 15mA$	110			dB
	A_{OL} $(V-) + 0.6V \leq V_O \leq (V+) - 0.6V$ $15mA \leq I_O \leq 30mA$	103			dB
FREQUENCY RESPONSE					
Gain-Bandwidth Product	GBW $G = 100$ $G = 1$		80 45		MHz MHz
Slew Rate	SR		27		V/ μs
Settling Time, 0.01%	t_s $V_S = \pm 15V, G = -1, 10V$ Step, $C_L = 100pF$		400		ns
0.0015% (16-bit)	$V_S = \pm 15V, G = -1, 10V$ Step, $C_L = 100pF$		700		ns
Overload Recovery Time	$G = -10$		500		ns
Total Harmonic Distortion + Noise	THD+N $G = +1, f = 1kHz,$ $V_O = 3V_{RMS}, R_L = 600\Omega$		0.000015 -136		% dB

ELECTRICAL CHARACTERISTICS: $V_S = \pm 2.25V$ to $\pm 18V$ (continued)
BOLDFACE limits apply over the specified temperature range, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$.

 At $T_A = +25^\circ\text{C}$ and $R_L = 10\text{k}\Omega$, unless otherwise noted.

PARAMETER	CONDITIONS	Standard Grade OPA211A, OPA2211A			UNIT	
		MIN	TYP	MAX		
OUTPUT						
Voltage Output	V_{OUT}	$R_L = 10\text{k}\Omega$, $A_{OL} \geq 114\text{dB}$	$(V-) + 0.2$		$(V+) - 0.2$	V
		$R_L = 600\Omega$, $A_{OL} \geq 110\text{dB}$	$(V-) + 0.6$		$(V+) - 0.6$	V
		$I_O < 25\text{mA}$, $A_{OL} \geq 110\text{dB}$	$(V-) + 0.6$		$(V+) - 0.6$	V
Short-Circuit Current	I_{SC}			+30/–45		mA
Capacitive Load Drive	C_{LOAD}		See Typical Characteristics			pF
Open-Loop Output Impedance	Z_O	1MHz		5		Ω
SHUTDOWN						
Shutdown Pin Input Voltage		Device shutdown	$(V+) - 0.35$			V
		Device enabled			$(V+) - 3$	V
POWER SUPPLY						
Specified Voltage	V_S		± 2.25		± 18	V
Quiescent Current (per channel)	I_Q	$I_{OUT} = 0\text{A}$		3.6	4.5	mA
Over Temperature					6	mA
TEMPERATURE RANGE						
Specified Range		T_A	–40		+125	$^\circ\text{C}$
Operating Range		T_A	–55		+150	$^\circ\text{C}$
Thermal Resistance						
DFN (3mm × 3mm)	θ_{JA}	Soldered to approximately 5cm × 5cm copper area		65		$^\circ\text{C/W}$
	θ_{JC}			57		$^\circ\text{C/W}$
MSOP-8	θ_{JA}			200		$^\circ\text{C/W}$
SO-8	θ_{JA}			150		$^\circ\text{C/W}$
SO-8 PowerPAD	θ_{JA}	Test board 1in × 0.5in heat-spreader, 1oz copper		52		$^\circ\text{C/W}$
	θ_{JC}			43		$^\circ\text{C/W}$

TYPICAL CHARACTERISTICS

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

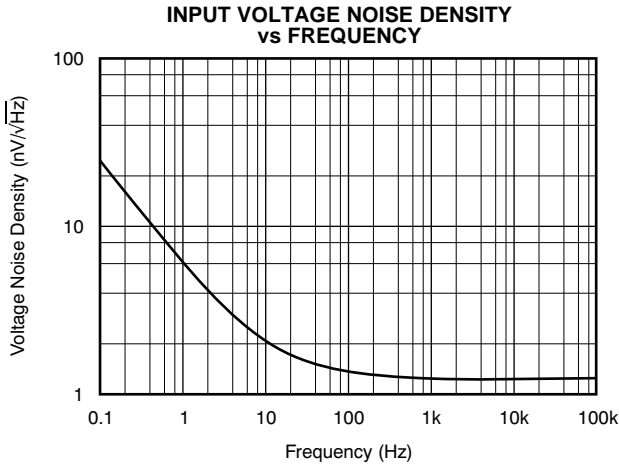


Figure 1.

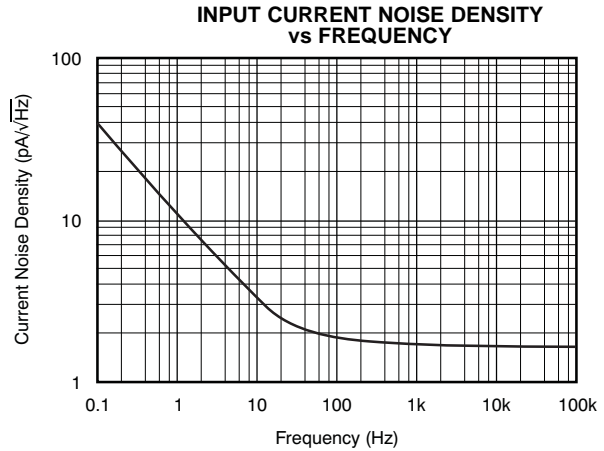


Figure 2.

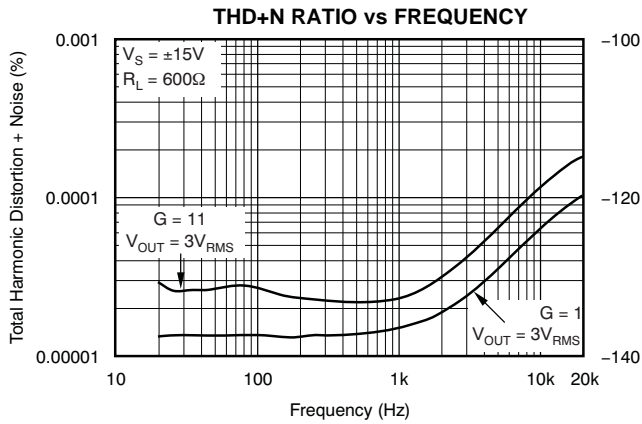


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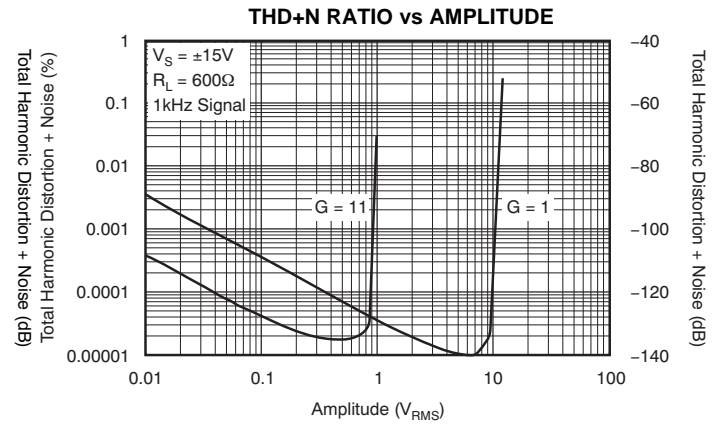


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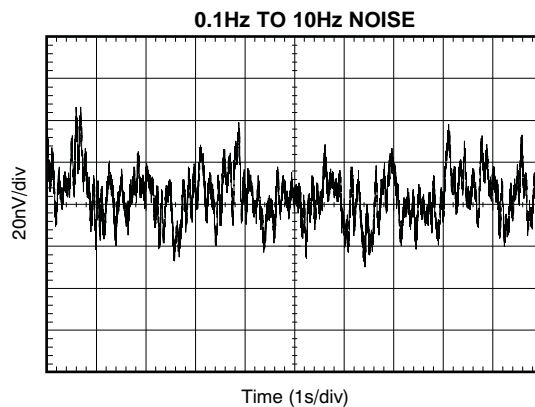


Figure 5.

TYPICAL CHARACTERISTICS (continued)

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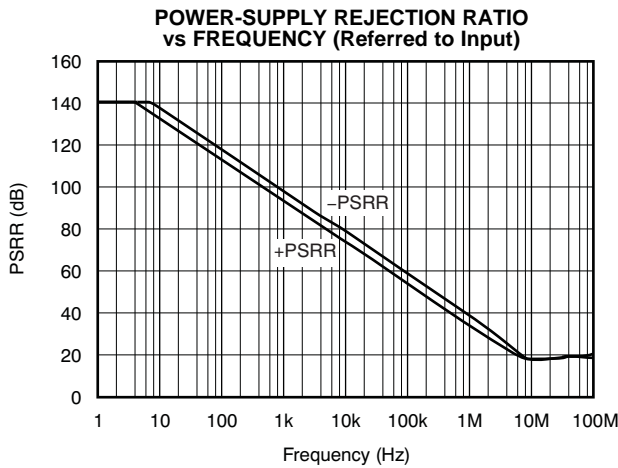


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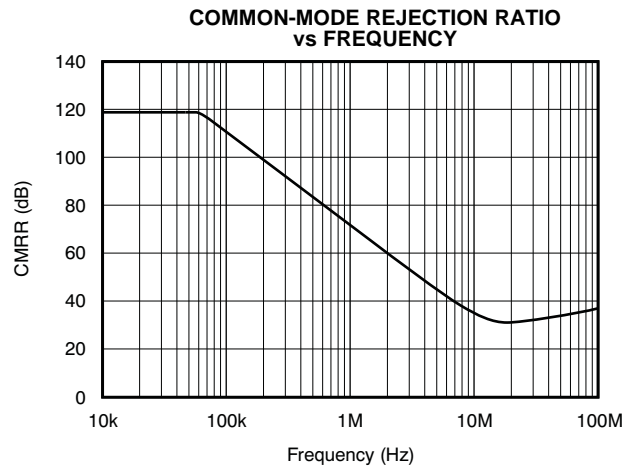


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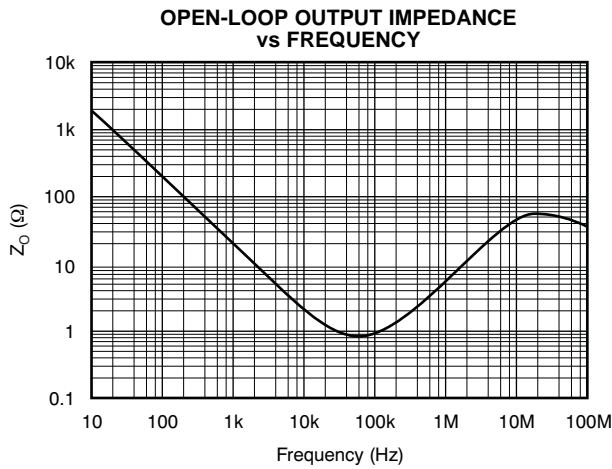


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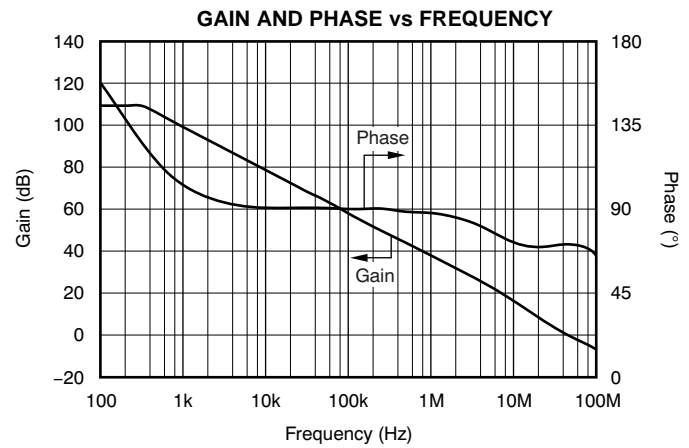


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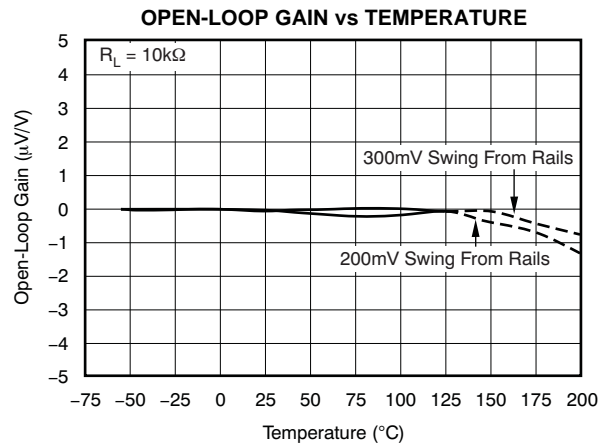


Figure 10.

TYPICAL CHARACTERISTICS (continued)

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

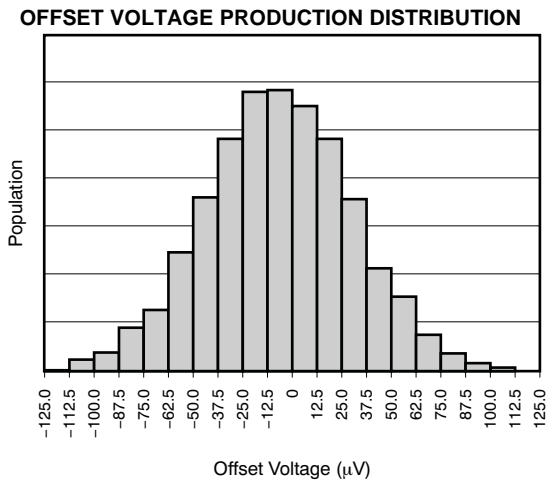


Figure 11.

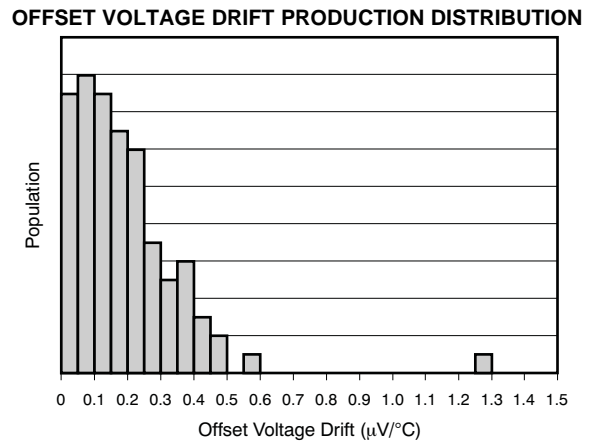


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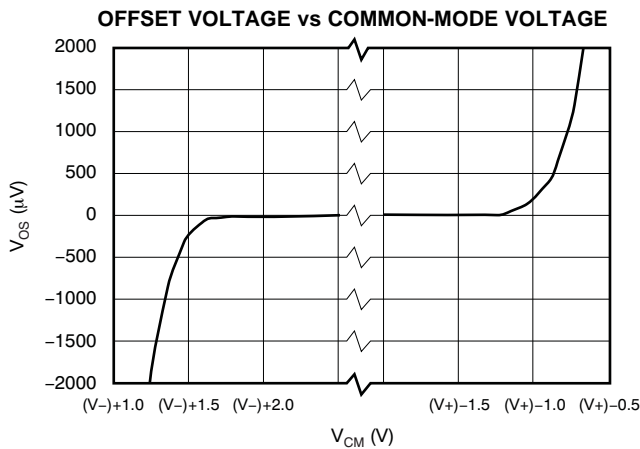


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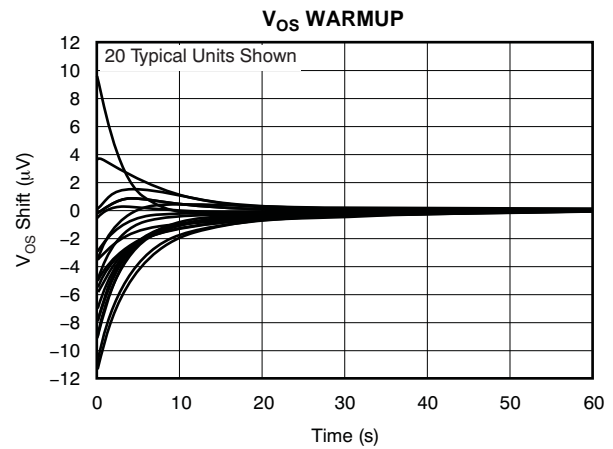


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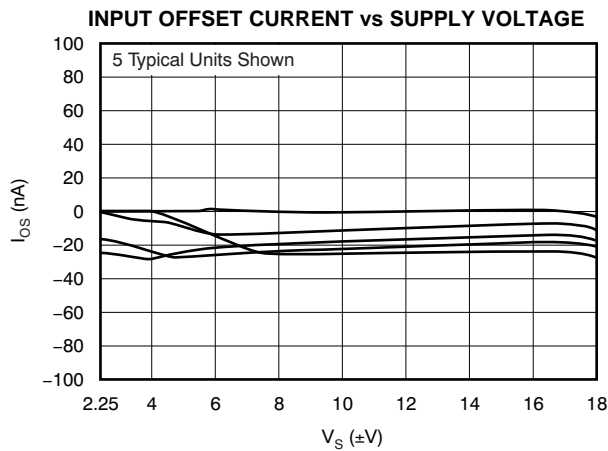


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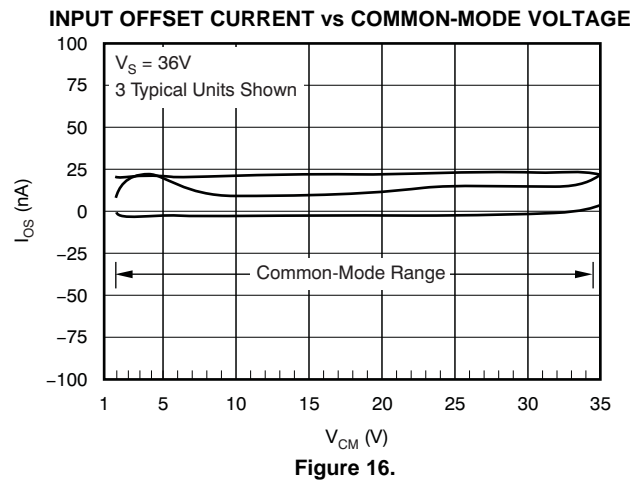


Figure 16.

TYPICAL CHARACTERISTICS (continued)

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.

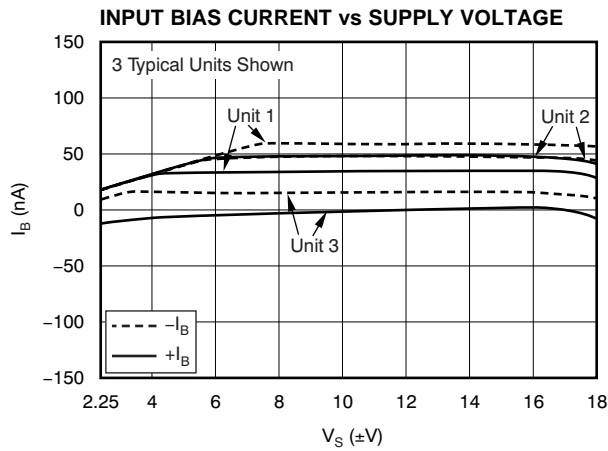


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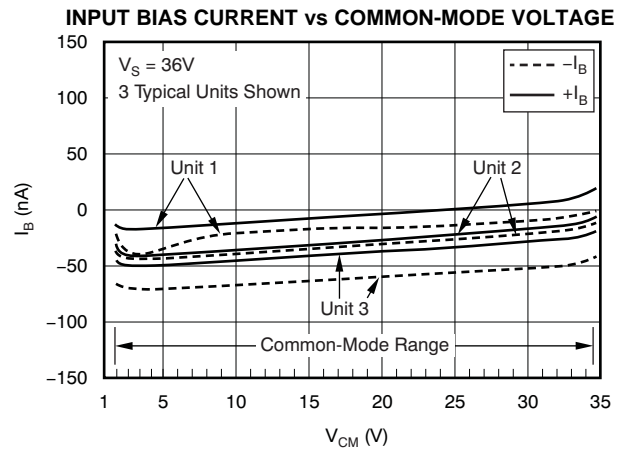


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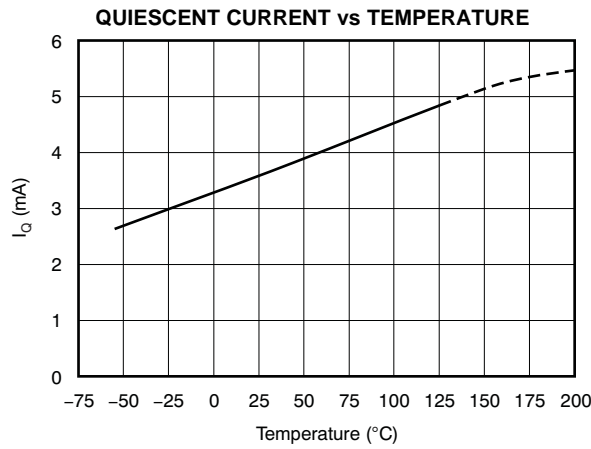


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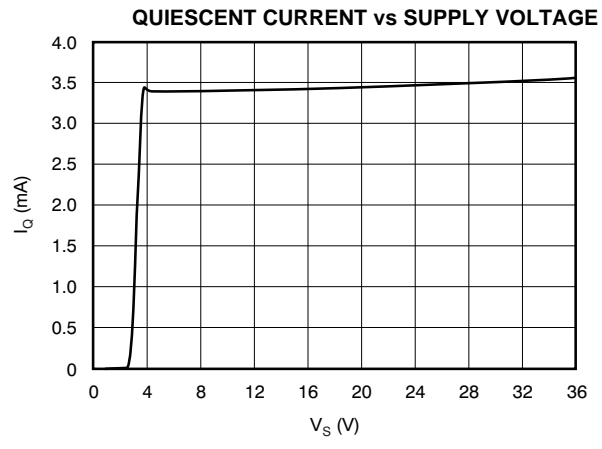


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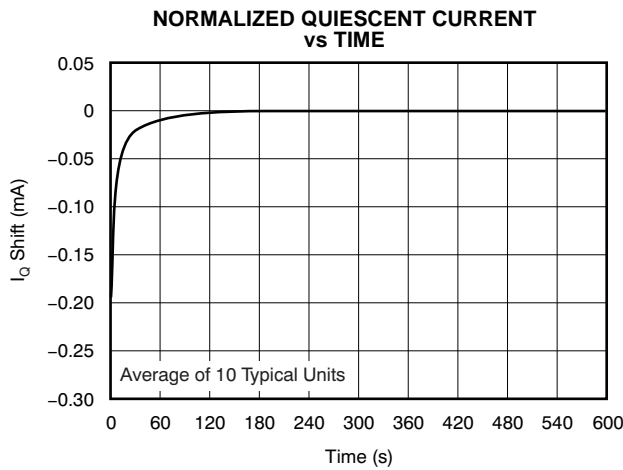


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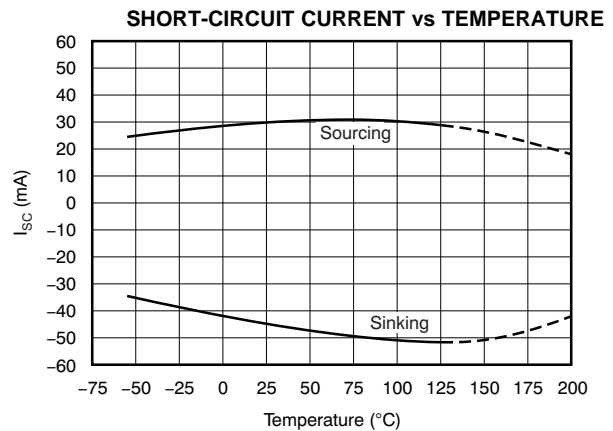
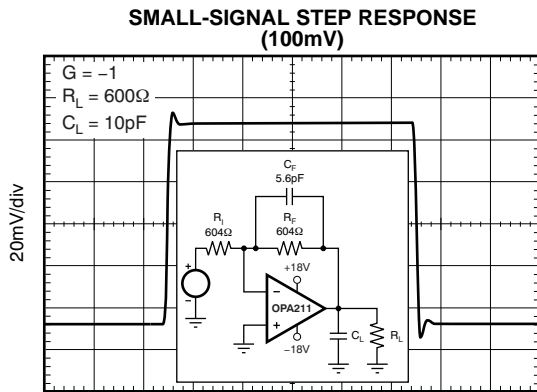


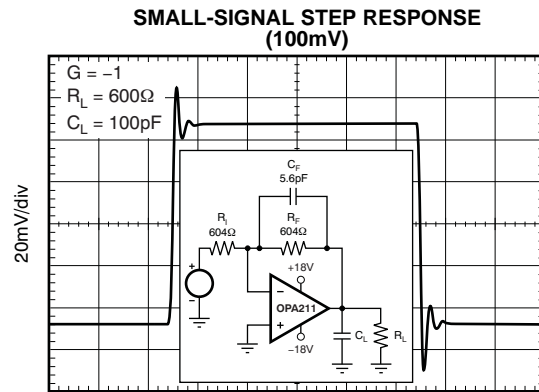
Figure 22.

TYPICAL CHARACTERISTICS (continued)

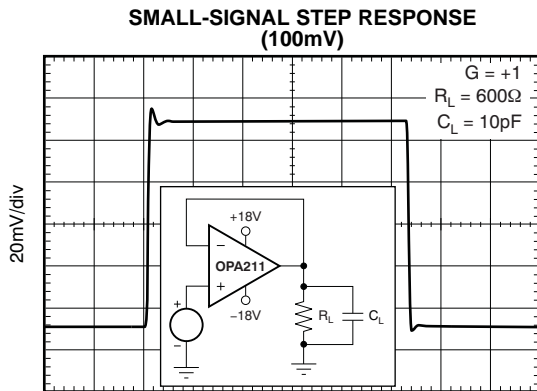
At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.



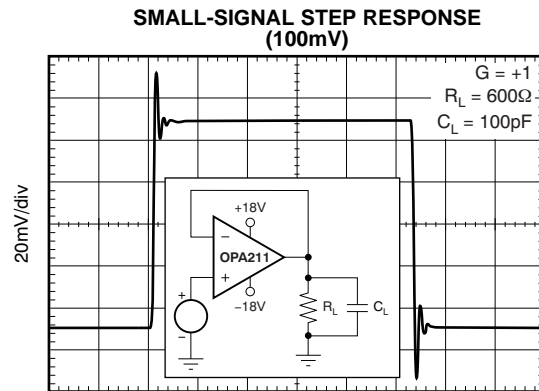
Time (0.1 $\mu\text{s}/\text{div}$)
Figure 23.



Time (0.1 $\mu\text{s}/\text{div}$)
Figure 24.



Time (0.1 $\mu\text{s}/\text{div}$)
Figure 25.



Time (0.1 $\mu\text{s}/\text{div}$)
Figure 26.

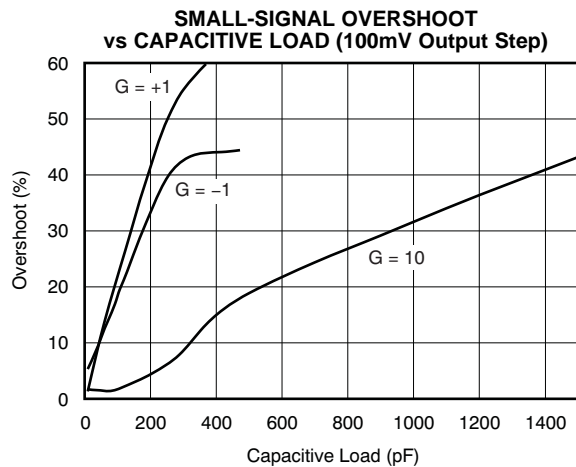


Figure 27.

TYPICAL CHARACTERISTICS (continued)

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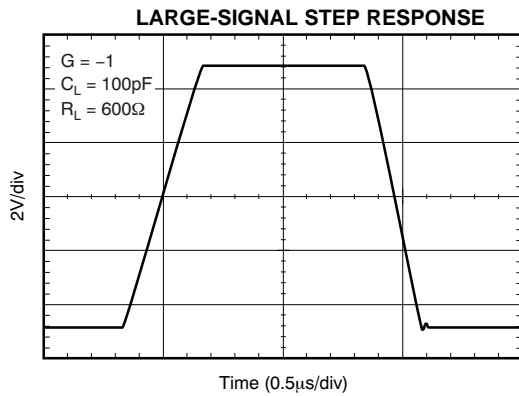


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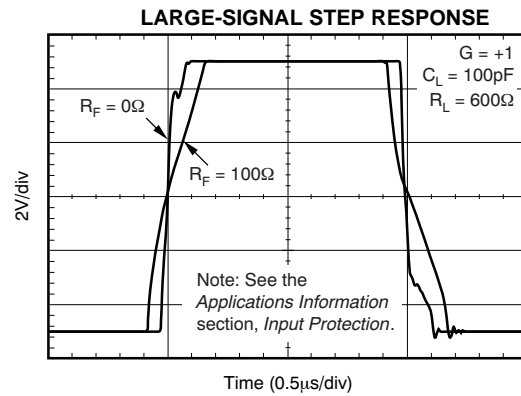


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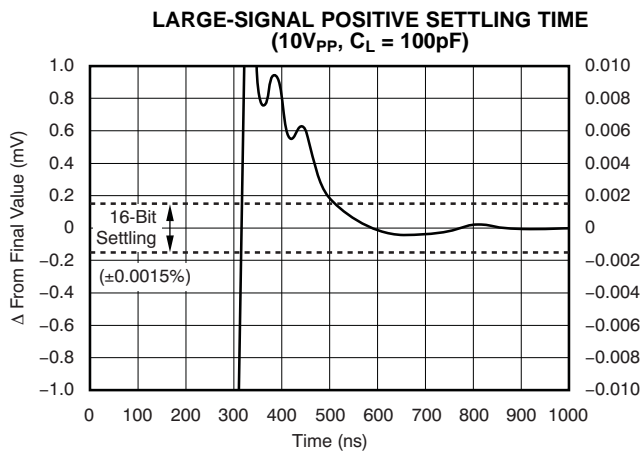


Figure 30.

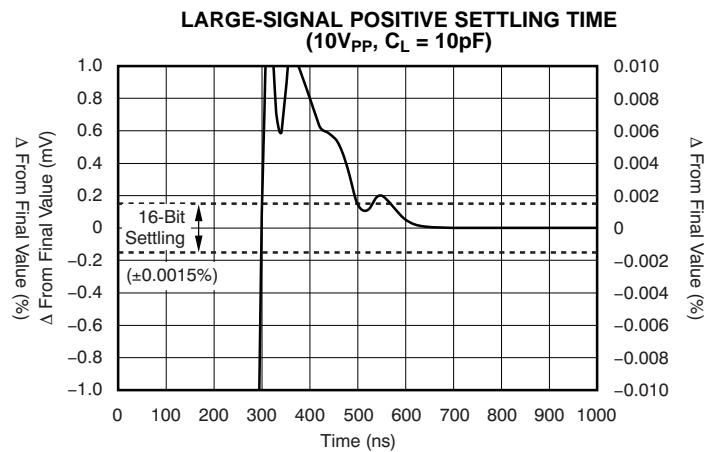


Figure 31.

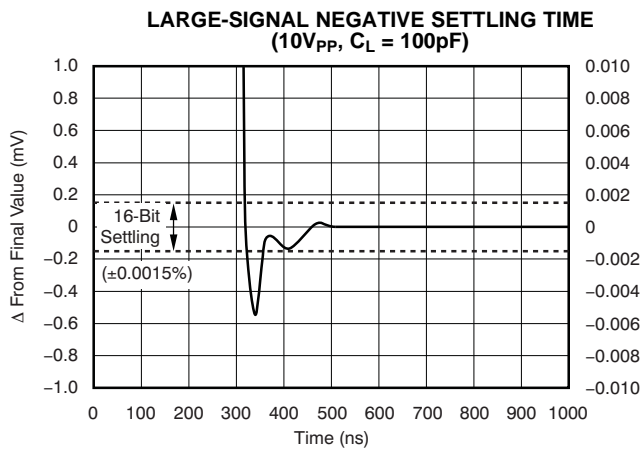


Figure 32.

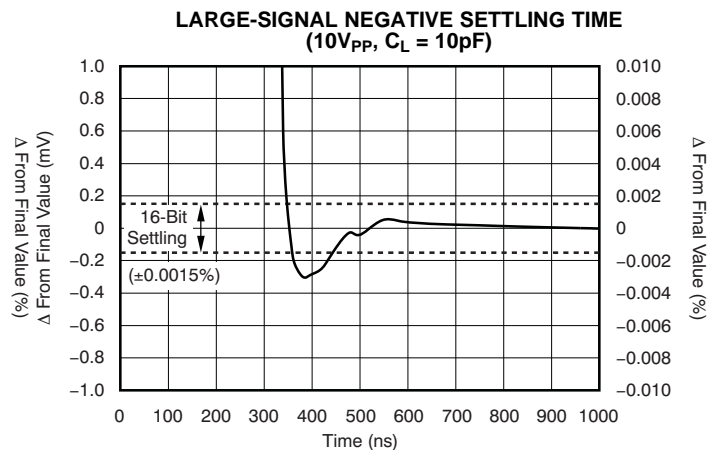
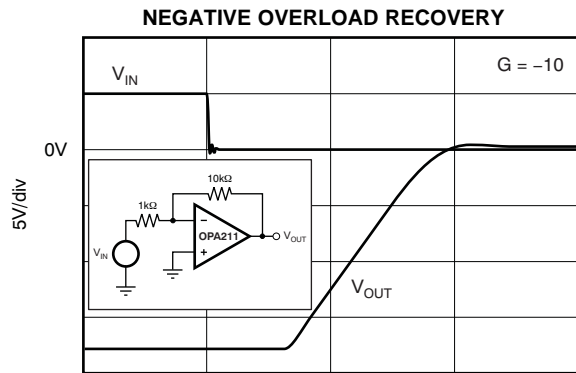


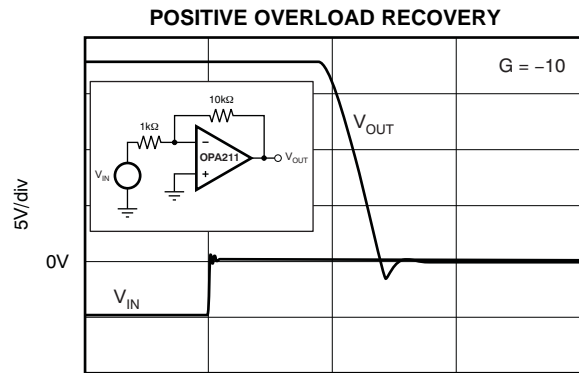
Figure 33.

TYPICAL CHARACTERISTICS (continued)

At $T_A = +25^\circ\text{C}$, $V_S = \pm 18\text{V}$, and $R_L = 10\text{k}\Omega$, unless otherwise noted.



Time (0.5μs/div)
Figure 34.



Time (0.5μs/div)
Figure 35.

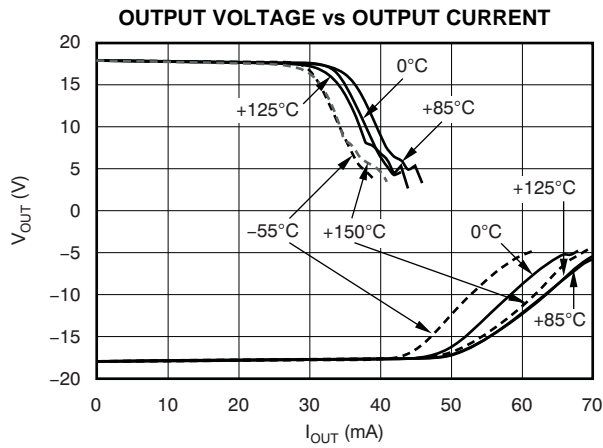


Figure 36.

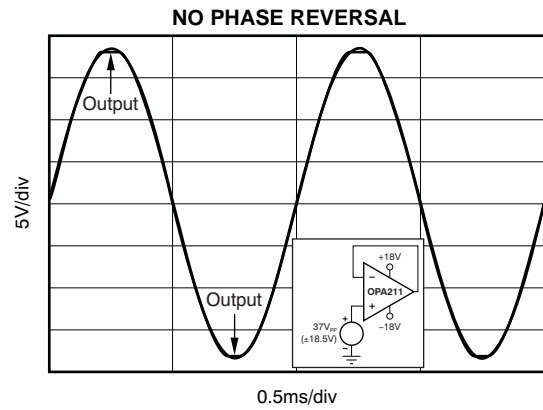


Figure 37.

APPLICATION INFORMATION

The OPA211 and OPA2211 are unity-gain stable, precision op amps with very low noise. Applications with noisy or high impedance power supplies require decoupling capacitors close to the device pins. In most cases, 0.1 μ F capacitors are adequate. [Figure 38](#) shows a simplified schematic of the OPA211. This die uses a SiGe bipolar process and contains 180 transistors.

OPERATING VOLTAGE

OPA211 series op amps operate from ± 2.25 V to ± 18 V supplies while maintaining excellent performance. The OPA211 series can operate with as little as +4.5V between the supplies and with up to +36V between the supplies. However, some applications do not require equal positive and

negative output voltage swing. With the OPA211 series, power-supply voltages do not need to be equal. For example, the positive supply could be set to +25V with the negative supply at -5V or vice-versa.

The common-mode voltage must be maintained within the specified range. In addition, key parameters are assured over the specified temperature range, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$. Parameters that vary significantly with operating voltage or temperature are shown in the [Typical Characteristics](#).

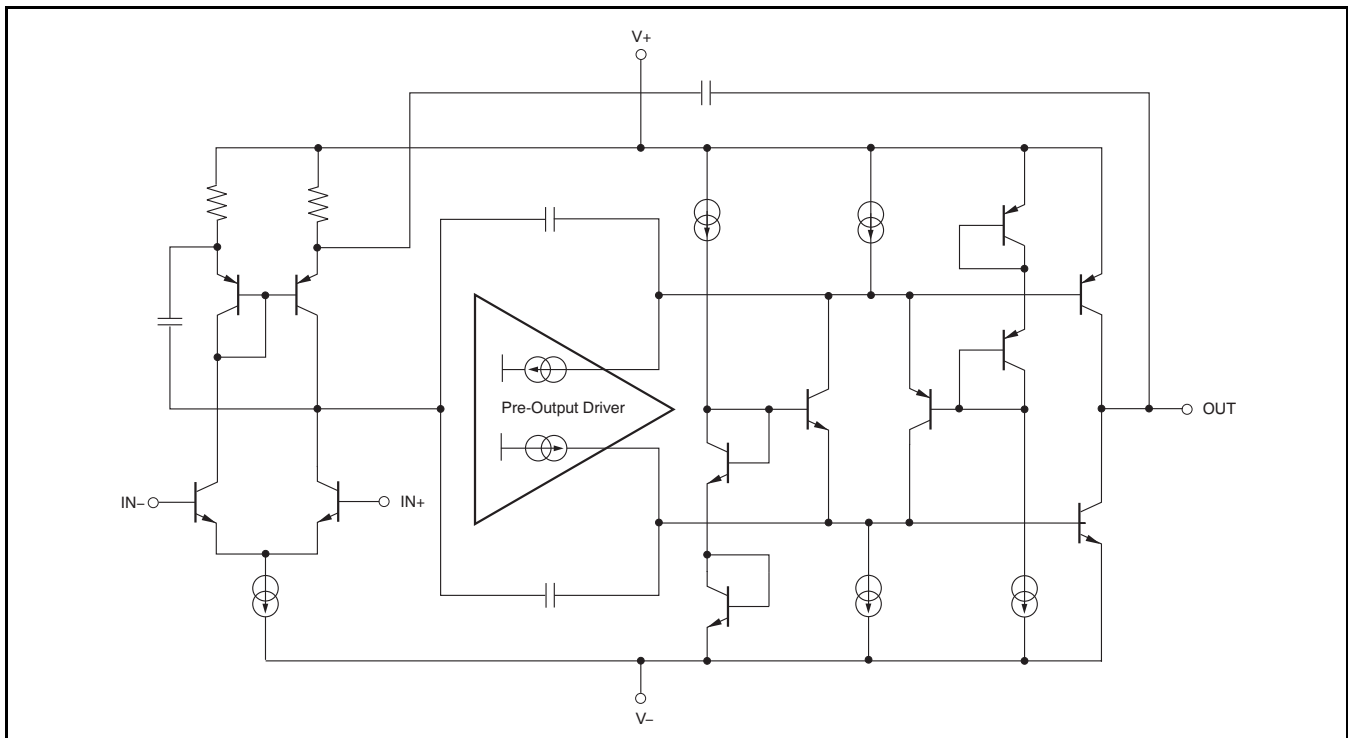


Figure 38. OPA211 Simplified Schematic

INPUT PROTECTION

The input terminals of the OPA211 are protected from excessive differential voltage with back-to-back diodes, as shown in Figure 39. In most circuit applications, the input protection circuitry has no consequence. However, in low-gain or $G = 1$ circuits, fast ramping input signals can forward bias these diodes because the output of the amplifier cannot respond rapidly enough to the input ramp. This effect is illustrated in Figure 29 of the Typical Characteristics. If the input signal is fast enough to create this forward bias condition, the input signal current must be limited to 10mA or less. If the input signal current is not inherently limited, an input series resistor can be used to limit the signal input current. This input series resistor degrades the low noise performance of the OPA211. See the [Noise Performance](#) section of this data sheet for further information on noise calculation. Figure 39 shows an example implementing a current-limiting feedback resistor.

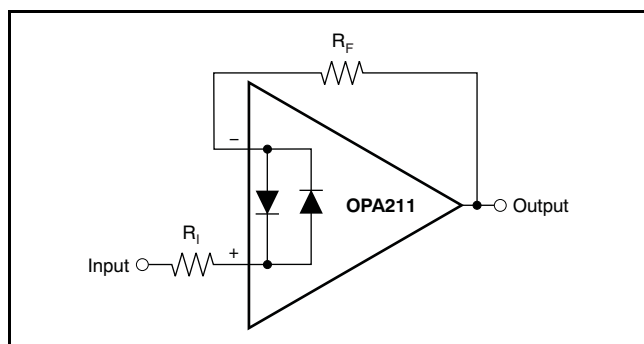


Figure 39. Pulsed Operation

NOISE PERFORMANCE

Figure 40 shows total circuit noise for varying source impedances with the op amp in a unity-gain configuration (no feedback resistor network, and therefore no additional noise contributions). Two different op amps are shown with total circuit noise calculated. The OPA211 has very low voltage noise, making it ideal for low source impedances (less than 2k Ω). A similar precision op amp, the OPA227, has somewhat higher voltage noise but lower current noise. It provides excellent noise performance at moderate source impedance (10k Ω to 100k Ω). Above 100k Ω , a FET-input op amp such as the OPA132 (very low current noise) may provide improved performance. The equation in Figure 40 is shown for the calculation of the total circuit noise. Note that e_n = voltage noise, i_n = current noise, R_S = source impedance, k = Boltzmann's constant = 1.38×10^{-23} J/K, and T is temperature in K. For more details on calculating noise, see the [Basic Noise Calculations](#) section.

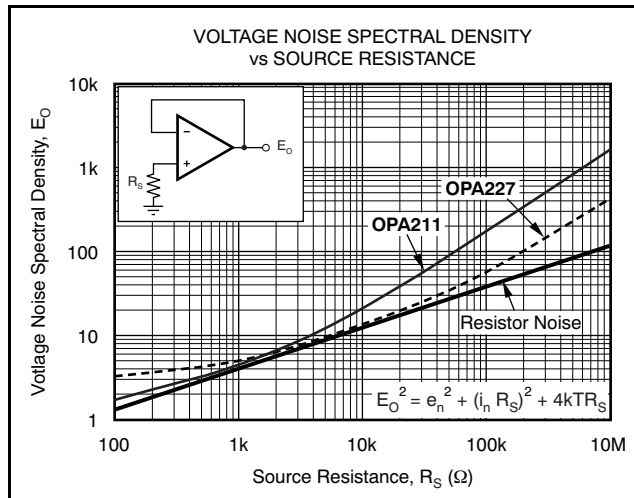


Figure 40. Noise Performance of the OPA211 in Unity-Gain Buffer Configuration

BASIC NOISE CALCULATIONS

Design of low-noise op amp circuits requires careful consideration of a variety of possible noise contributors: noise from the signal source, noise generated in the op amp, and noise from the feedback network resistors. The total noise of the circuit is the root-sum-square combination of all noise components.

The resistive portion of the source impedance produces thermal noise proportional to the square root of the resistance. This function is plotted in Figure 40. The source impedance is usually fixed; consequently, select the op amp and the feedback resistors to minimize the respective contributions to the total noise.

Figure 40 depicts total noise for varying source impedances with the op amp in a unity-gain configuration (no feedback resistor network, and therefore no additional noise contributions). The operational amplifier itself contributes both a voltage noise component and a current noise component. The voltage noise is commonly modeled as a time-varying component of the offset voltage. The current noise is modeled as the time-varying component of the input bias current and reacts with the source resistance to create a voltage component of noise. Therefore, the lowest noise op amp for a given application depends on the source impedance. For low source impedance, current noise is negligible and voltage noise generally dominates. For high source impedance, current noise may dominate.

Figure 41 illustrates both inverting and noninverting op amp circuit configurations with gain. In circuit configurations with gain, the feedback network resistors also contribute noise. The current noise of the op amp reacts with the feedback resistors to create additional noise components. The feedback resistor values can generally be chosen to make these noise sources negligible. The equations for total noise are shown for both configurations.

TOTAL HARMONIC DISTORTION MEASUREMENTS

OPA211 series op amps have excellent distortion characteristics. THD + Noise is below 0.0001% ($G = +1$, $V_O = 3V_{RMS}$) throughout the audio frequency range, 20Hz to 20kHz, with a 600Ω load.

The distortion produced by OPA211 series op amps is below the measurement limit of many commercially available equipment. However, a special test circuit illustrated in Figure 42 can be used to extend the measurement capabilities.

Op amp distortion can be considered an internal error source that can be referred to the input. Figure 42 shows a circuit that causes the op amp distortion to be 101 times greater than normally produced by the op amp. The addition of R_3 to the otherwise standard noninverting amplifier configuration alters the

feedback factor or noise gain of the circuit. The closed-loop gain is unchanged, but the feedback available for error correction is reduced by a factor of 101, thus extending the resolution by 101. Note that the input signal and load applied to the op amp are the same as with conventional feedback without R_3 . The value of R_3 should be kept small to minimize its effect on the distortion measurements.

Validity of this technique can be verified by duplicating measurements at high gain and/or high frequency where the distortion is within the measurement capability of the test equipment. Measurements for this data sheet were made with an Audio Precision System Two distortion/noise analyzer, which greatly simplifies such repetitive measurements. The measurement technique can, however, be performed with manual distortion measurement instruments.

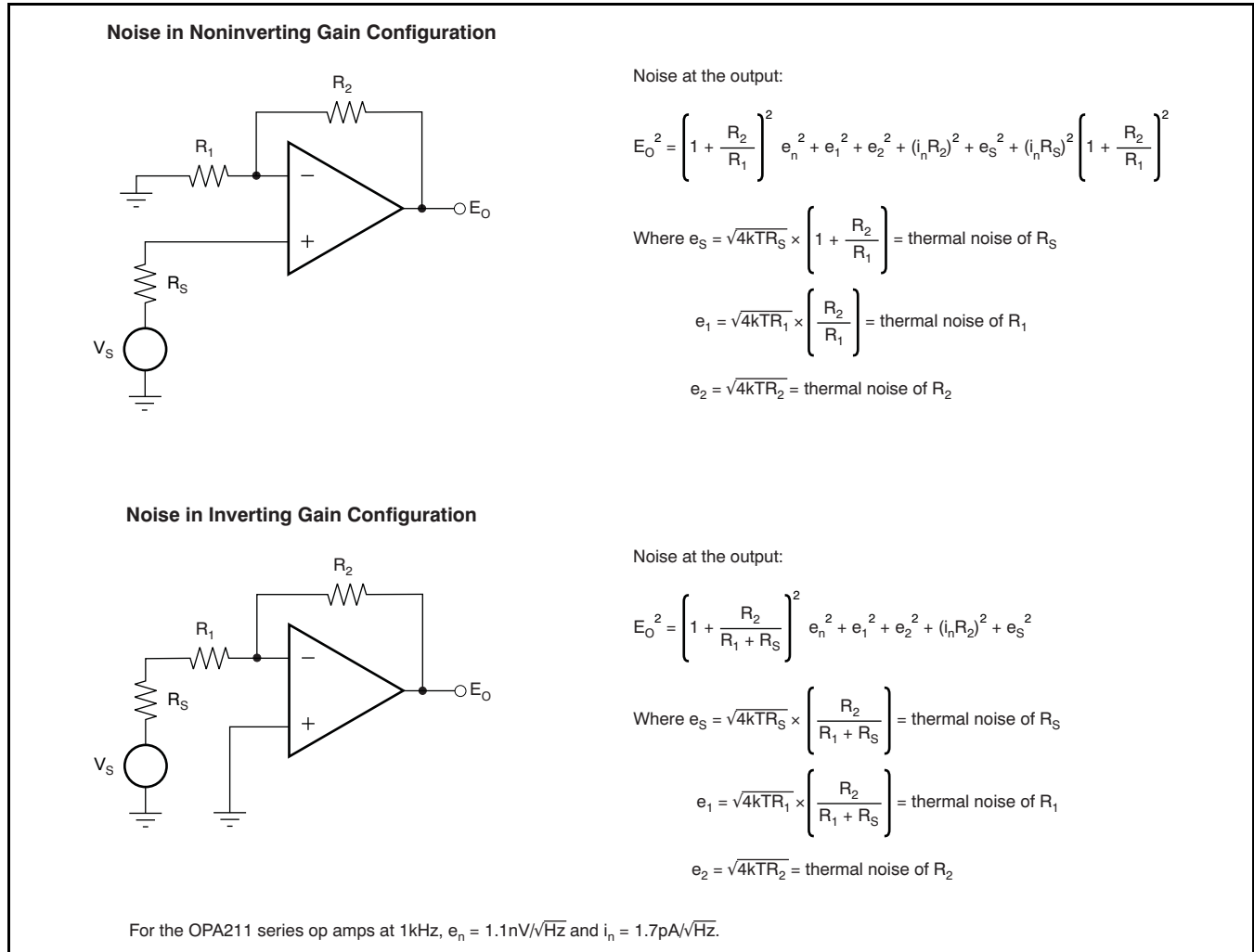


Figure 41. Noise Calculation in Gain Configurations

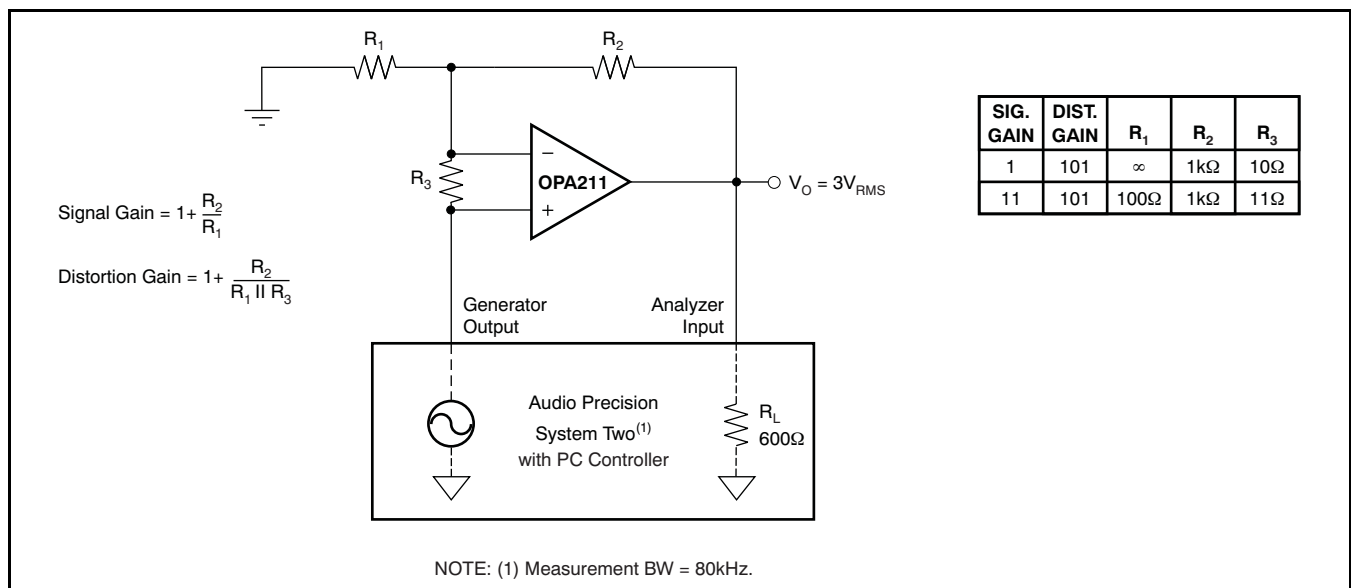


Figure 42. Distortion Test Circuit

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